

1. For a bicycle model, the linearized equations are $M\ddot{q} + vC_1\dot{q} + [gK_0 + v^2 K_2]q = f$, where $q = [\phi, \delta]', f = [T_\phi, T_\delta]', M = \begin{bmatrix} 80.8 & 2.3 \\ 2.3 & 0.3 \end{bmatrix}$, $g = 9.8$, $v = 2$, $C_1 = \begin{bmatrix} 0 & 33.9 \\ -0.9 & 1.7 \end{bmatrix}$, $K_0 = \begin{bmatrix} -81 & -2.6 \\ -2.6 & -0.8 \end{bmatrix}$, $K_2 = \begin{bmatrix} 0 & 76.6 \\ 0 & 2.7 \end{bmatrix}$.

(T_ϕ is lean torque, T_δ is steering torque)

- a) Using $x = [\phi \ \delta \ \dot{\phi} \ \dot{\delta}]'$, $u = f$, write the state-space model $\dot{x} = Ax + Bu$. $A = ?$, $B = ?$
- b) Is the system controllable using the input T_ϕ only ($T_\delta \equiv 0$, it is not there).
- c) Is the system controllable using the input T_δ only ($T_\phi \equiv 0$, it is not there).

a) $x_1 = \phi, x_2 = \delta, x_3 = \dot{\phi}, x_4 = \dot{\delta}$
 $\Rightarrow \dot{x}_1 = x_3, \dot{x}_2 = x_4$

$$\begin{aligned} M\ddot{q} + vC_1\dot{q} + [gK_0 + v^2 K_2]q &= f \\ \Rightarrow M \begin{bmatrix} \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} + vC_1 \begin{bmatrix} x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} gK_0 + v^2 K_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} &= u \\ \Rightarrow M \begin{bmatrix} \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} &= -[gK_0 + v^2 K_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} - vC_1 \begin{bmatrix} x_3 \\ x_4 \end{bmatrix} + u \\ \Rightarrow \begin{bmatrix} \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} &= -M^{-1} [gK_0 + v^2 K_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} - M^{-1} v C_1 \begin{bmatrix} x_3 \\ x_4 \end{bmatrix} + M^{-1} u \end{aligned}$$

$$\therefore \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\frac{1}{M^{-1}}x & -\frac{1}{M^{-1}}x & 0 & 0 \\ [EgK_0 + v^2 K_2] & 1 - M^{-1}x & vC_1 & 0 \end{bmatrix}}_A \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ -\frac{1}{M^{-1}} & 0 \end{bmatrix}}_B u$$

Numerical values are, $M = \begin{bmatrix} 80.8 & 2.3 \\ 2.3 & 0.3 \end{bmatrix}$, $g = 9.8$, $v = 2$, $C_1 = \begin{bmatrix} 0 & 33.9 \\ -0.9 & 1.7 \end{bmatrix}$, $K_0 = \begin{bmatrix} -81 & -2.6 \\ -2.6 & -0.8 \end{bmatrix}$, $K_2 = \begin{bmatrix} 0 & 76.6 \\ 0 & 2.7 \end{bmatrix}$.

$$\begin{aligned} M^{-1} &= \frac{1}{80.8 \times 0.3 - (2.3)^2} \begin{bmatrix} 0.3 & -2.3 \\ -2.3 & 80.8 \end{bmatrix} \\ &= 0.053 \begin{bmatrix} 0.016 & -0.122 \\ -0.122 & 4.28 \end{bmatrix} = \begin{bmatrix} 0.016 & -0.122 \\ -0.122 & 4.28 \end{bmatrix} \\ M^{-1}vC_1 &= 2 \begin{bmatrix} 0.016 & -0.122 \\ -0.122 & 4.28 \end{bmatrix} \begin{bmatrix} 0 & 33.9 \\ -0.9 & 1.7 \end{bmatrix} \\ &= \begin{bmatrix} 2(0.122 \times 0.9) & 2(0.016 \times 33.9 - 0.122 \times 1.7) \\ -2 \times 4.28 \times 0.9 & -2(33.9 \times 0.122 - 4.28 \times 1.7) \end{bmatrix} \\ &= \begin{bmatrix} 0.22 & 0.67 \\ -7.7 & 6.28 \end{bmatrix} \end{aligned}$$

$$\bar{M}^{-1} [gK_0 + v^2 K_2] = \bar{M}^{-1} \left(\begin{bmatrix} -81 \times 9.8 & -2.6 \times 9.8 \\ -2.6 \times 9.8 & -0.8 \times 9.8 \end{bmatrix} + \begin{bmatrix} 306.4 & 4 \times 76.6 \\ 0 & 4 \times 2.7 \end{bmatrix} \right)$$

$$= \begin{bmatrix} 0.016 & -0.122 \\ -0.122 & 4.28 \end{bmatrix} \begin{bmatrix} -793.8 & 280.92 \\ -25.48 & 2.96 \end{bmatrix}$$

$$= \begin{bmatrix} -0.016 \times 793.8 + 0.122 \times 25.48 & 280.92 \times 0.016 \\ 12.7 & 3.12 \\ 0.122 \times 793.8 - 4.28 \times 25.48 & -280.92 \times 0.122 \\ 96.8 & 109.05 \\ 4.49 & 0.36 \\ 34.27 & 12.67 \end{bmatrix}$$

$$= \begin{bmatrix} -9.58 & 4.13 \\ -12.25 & -21.6 \end{bmatrix}$$

$$A = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 9.58 & -4.13 & -0.22 & -0.67 \\ 12.25 & 21.6 & 7.7 & -6.28 \end{bmatrix}$$

$$B = \begin{bmatrix} b_1 & | & b_2 \\ 0 & | & 0 \\ 0 & | & 0 \\ 0.016 & | & -0.122 \\ -0.122 & | & 4.28 \end{bmatrix}$$

b) & c) check
rank $[b_i \ A b_i \ A^2 b_i \ A^3 b_i] = 4$
i=1 for b)
i=2 for c)

2. A and B are square matrices.

- a) Show that, if $AB = BA$, $e^{A+B} = e^A \cdot e^B$.
- b) By counterexample, choose A and B such that $AB \neq BA$ and check that $e^{A+B} \neq e^A \cdot e^B$

a) $e^{A+B} = I + (A+B) + \frac{(A+B)^2}{2!} + \frac{(A+B)^3}{3!} + \dots$

$$e^A = I + A + \frac{A^2}{2!} + \frac{A^3}{3!} + \dots$$

$$e^B = I + B + \frac{B^2}{2!} + \frac{B^3}{3!} + \dots$$

$$e^A \cdot e^B = I + (A+B) + \left(\frac{A^2}{2!} + \frac{B^2}{2!} + AB \right) + \dots$$

Now, $(A+B)^2 = (A+B)(A+B)$

$$= A^2 + AB + BA + B^2$$



If $AB = BA$, then $(A+B)^2 = A^2 + 2AB + B^2$
and $e^{A+B} = e^A \cdot e^B$

(similarly for higher powers of $(A+B)$)

b) $A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, B = \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix}$

$$AB = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, BA = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

Here $AB \neq BA$.

$$A+B = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}$$

$$e^A = I + A \quad \left[\because A^2 = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \right]$$
$$= \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \quad = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$e^B = I + B + \frac{B^2}{2!} + \dots \quad \left[B^2 = \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix} \right]$$

$$= I + B \left(1 + \frac{1}{2!} + \frac{1}{3!} + \dots \right) \quad = \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix} = B$$

$$= I + B(e-1)$$

$$= \begin{bmatrix} 1 & 1-e \\ 0 & e \end{bmatrix}$$

$$e^A \cdot e^B = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 1-e \\ 0 & e \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & e \end{bmatrix}$$

$$e^{A+B} = I + (A+B)(e-1) \quad \left[\because (A+B)^2 = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \right]$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & e \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}$$

3. A disastrous way to control an unstable system is to cancel the unstable pole with a zero. Consider a transfer function from input to output as $H(s) = \frac{1}{s^2 - \Omega^2}$

a) Is this unstable?

Consider a controller $G(s) = \frac{s - \bar{\Omega}}{s + \bar{\Omega}}$.

Clearly, $G(s)H(s) = \frac{1}{s^2 + \Omega^2}$ when $\Omega = \bar{\Omega}$.

When $\Omega \neq \bar{\Omega}$, the transfer function $G(s)H(s)$ can be shown to be in the form $\dot{x} = Ax + Bu$, where $A = \begin{bmatrix} 0 & 1 & 0 \\ -\Omega^2 & 0 & -1 \\ 0 & 0 & 0 \end{bmatrix}$, $B = \begin{bmatrix} 0 \\ 1 \\ \frac{1}{\bar{\Omega}} \end{bmatrix}$.

- b) Find the transformation T that diagonalizes A . $AT = TD$
- c) Express the equation in Z -coordinates, where $Z = T^{-1}x$. ($Z = [z_1, z_2, z_3]^T$)
- d) Analyze the Z -equations in the limit $\bar{\Omega} \rightarrow \Omega$. Can they be controlled?

a) Unstable as pole $= +1$ in RHP

b) eigenvalues of A ,

$$sI - A = \begin{bmatrix} s & -1 & 0 \\ -\Omega^2 & s & -1 \\ 0 & 0 & s \end{bmatrix}$$

$$\det(\delta I - A) = \delta (\delta^2 + \Omega^2)$$

\therefore eigenvalues are $\Omega, 0, -\Omega$

eigenvectors:

$$\underline{\delta = \Omega}, \quad \delta I - A = \begin{bmatrix} \Omega & -1 & 0 \\ -\Omega^2 & \Omega & 1 \\ 0 & 0 & \Omega \end{bmatrix}$$

$$\sim \begin{bmatrix} \Omega & -1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & \Omega \end{bmatrix} \sim \begin{bmatrix} \Omega & -1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\therefore \text{eigenvector can be } \begin{bmatrix} 1 \\ \Omega \\ 0 \end{bmatrix}$$

$$\underline{\delta = 0}, \quad \delta I - A = \begin{bmatrix} 0 & -1 & 0 \\ -\Omega^2 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\therefore \text{eigenvector can be } \begin{bmatrix} 1 \\ 0 \\ -\Omega^2 \end{bmatrix}$$

$$\underline{\delta = -\Omega}, \quad \delta I - A = \begin{bmatrix} -\Omega & -1 & 0 \\ -\Omega^2 & -\Omega & 1 \\ 0 & 0 & -\Omega \end{bmatrix}$$

$$\sim \begin{bmatrix} -\Omega & -1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & -\Omega \end{bmatrix} \sim \begin{bmatrix} \Omega & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix}$$

\therefore eigenvector can be $\begin{bmatrix} 1 \\ -\Omega \\ 0 \end{bmatrix}$

The transformation matrix, $T = \begin{bmatrix} 1 & 1 & 1 \\ \Omega & 0 & -\Omega \\ 0 & \Omega^2 & 0 \end{bmatrix}$

$$c) \dot{\vec{z}} = \vec{T}^{-1} \dot{\vec{x}}$$

$$= \vec{T}^{-1} \vec{A} \vec{T} \vec{z} + \vec{T}^{-1} \vec{B} u$$

$$\vec{T}^{-1} = \frac{\text{adj}(T)}{\det(T)}$$

$$\rightarrow \begin{bmatrix} \Omega & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & -\Omega \end{bmatrix}$$

$$\det(T) = -\Omega^2 \begin{vmatrix} 1 & 1 \\ -\Omega & -\Omega \end{vmatrix} = 2\Omega^3$$

$$\text{adj}(T) = \begin{bmatrix} \Omega^3 & 0 & \Omega^3 \\ \Omega^2 & 0 & -\Omega^2 \\ -\Omega & 2\Omega & -\Omega \end{bmatrix}^T = \begin{bmatrix} \Omega^3 & \Omega^2 & -\Omega \\ 0 & 0 & 2\Omega \\ \Omega^3 & -\Omega^2 & -\Omega \end{bmatrix}$$

$$\therefore \vec{T}^{-1} \vec{B} = \begin{bmatrix} \frac{1}{2} & \frac{1}{2\Omega} & -\frac{1}{2\Omega^2} \\ 0 & 0 & \frac{1}{\Omega^2} \\ \frac{1}{2} & -\frac{1}{2\Omega} & -\frac{1}{\Omega^2} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ \Omega \end{bmatrix} = \begin{bmatrix} \frac{1}{2\Omega^2}(\Omega - \bar{\Omega}) \\ \frac{\bar{\Omega}}{\Omega^2} \\ -\frac{1}{2\Omega^2}(\Omega + \bar{\Omega}) \end{bmatrix}$$

as $\bar{\Omega} \rightarrow \Omega$,

$$\begin{aligned}\dot{z}_1 &= \Omega z_1 + \underbrace{\frac{1}{2\Omega^2}(\Omega - \bar{\Omega})u}_{\text{pole-zero cancellation}} \\ \dot{z}_2 &= \frac{\bar{\Omega}}{\Omega^2}u \\ \dot{z}_3 &= -\Omega z_3 - \frac{1}{2\Omega^2}(\Omega + \bar{\Omega})u\end{aligned}$$

z_1 -equation is unstable and there is no input term