

# Tutorial - II

## EEL306 - Communication Engineering (II-Sem 2013-14)

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- 1) Find the complex baseband envelope of each of the following real-valued band-limited band-pass signals.

a)

$$x(t) = 0.5 \cos \left( 20000\pi t + \frac{\pi}{6} \right). \quad (1)$$

b)

$$x(t) = 0.25 \cos \left( 20000\pi t + \frac{\pi}{4} \right) + \sin \left( 20100\pi t - \frac{\pi}{3} \right). \quad (2)$$

c)

$$x(t) = 2 \cos \left( 50\pi t \right) \sin \left( 25000\pi t \right). \quad (3)$$

d)

$$x(t) = m(t) \sin \left( 2\pi f t + \phi \right), \quad (4)$$

where  $m(t)$  is a real-valued baseband signal bandlimited to  $[-W, W]$ , and  $\phi \in [-\pi, \pi)$  is a constant.

- 2) If  $\tilde{x}(t)$  is the complex baseband envelope of the real-valued bandpass signal  $x(t)$ , then find an expression for the complex baseband envelope of  $y(t) = x(t - \tau)$  in terms of  $\tilde{x}(t)$ .
- 3) Before transmitting the real-valued band-limited bandpass signal  $s(t)$ , one would like to pass it through a bandpass filter (having impulse response  $h(t)$ ) (This is usually done in order to adhere to radiation constraints specified by standards/regulatory bodies). The filtered output is given by

$$x(t) = \int_{-\infty}^{\infty} h(\tau) s(t - \tau) d\tau. \quad (5)$$

In practice, filtering of the transmit signal is not done in pass band, but in baseband due to implementation related issues (low cost, low power consumption). Let  $s(t) = \text{sinc}(2Wt) \cos(2\pi f_c t)$  and  $h(t) = \text{sinc}^2(2Wt) \sin(2\pi f_c t)$ .

Derive an expression for the impulse response of the equivalent complex baseband filter ( $h_b(t)$ ) such that

$$\tilde{x}(t) = \int_{-\infty}^{\infty} h_b(\tau) \tilde{s}(t - \tau) d\tau, \quad (6)$$

i.e., we can get the same output  $x(t)$  in (5) by simply filtering  $\tilde{s}(t)$  in complex baseband followed by an upconversion (no need for any filtering in pass band).

Finally derive an expression for  $x(t)$  (first derive an expression for  $\tilde{x}(t)$ ).

#### 4) (Group/Envelope delay and Phase delay)

The signal received at the receiver ( $y(t)$ ) is usually passed through a band pass filter  $h(t)$  to get rid of out of band interference (i.e., outside the band  $[f_c - W, f_c + W]$ ). Assuming that  $y(t)$  is narrow band (i.e.,  $f_c \gg W$ , the in-band phase response of  $h(t)$  is almost linear, and  $|H(f)| \approx |H(f_c)|$  inside the pass band  $|f - f_c| < W$ ), you are required to show that the filtered output  $z(t)$  is given by

$$z(t) \approx |H(f_c)| \operatorname{Re}\left(\tilde{y}(t - t_g) e^{j2\pi f_c(t - t_p)}\right), \quad (7)$$

$$\begin{aligned} t_g &\triangleq -\frac{1}{2\pi} \frac{d\theta(f)}{df} \Big|_{f=f_c} \\ t_p &\triangleq -\frac{1}{2\pi} \frac{\theta(f_c)}{f_c} \end{aligned} \quad (8)$$

where  $\theta(f) \triangleq \arg\left(H(f)/|H(f)|\right)$  is the phase response of  $h(t)$ . Since the signal  $y(t)$  is narrow band we can assume that inside the pass band

$$\theta(f) \approx \theta(f_c) + (f - f_c) \frac{d\theta(f)}{df} \Big|_{f=f_c}. \quad (9)$$

Note that this is the first order Taylor series expansion of  $\theta(f)$  around  $f = f_c$ .

From (7) it can be concluded that, due to band pass filtering the complex envelope of the received signal gets delayed by  $t_g$ , whereas the carrier signals  $\cos(2\pi f_c t)$  and  $\sin(2\pi f_c t)$  are delayed by  $t_p$  seconds.