

fig. 1

Understanding,

At low frequency you see two stages
 & at high frequency one of the stage is shorted out.

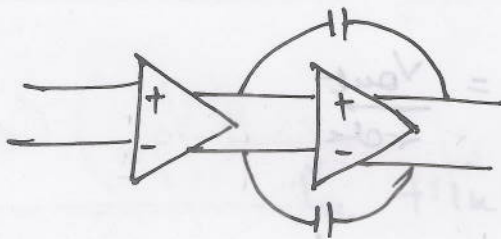


fig. 2

or provide alternate path.
 for low frequency.

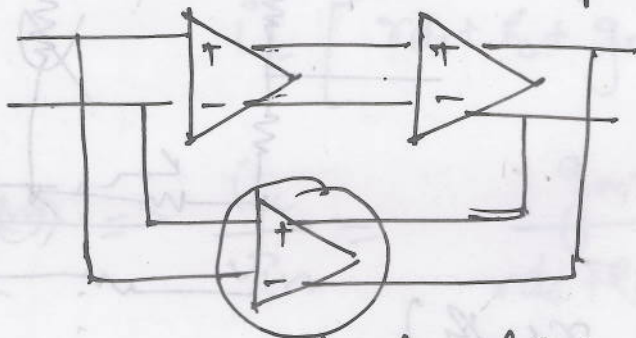


fig 3.

for high frequency

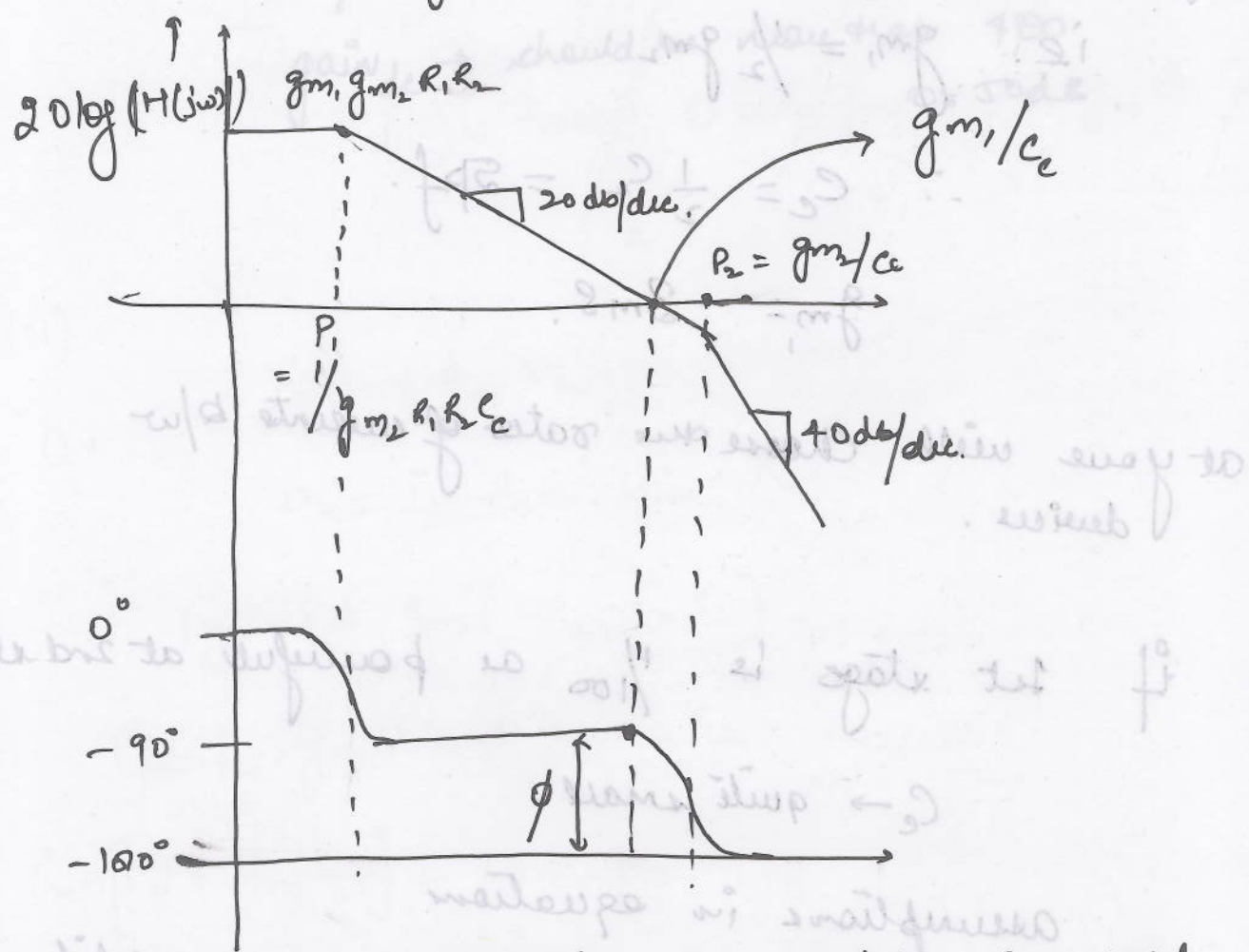
Analyzing figure I

$$R_2 \rightarrow g_{m2}/C_L$$

$$P_1 \rightarrow \frac{1}{g_{m2} R_1 R_2 C_L}$$

$$\frac{g_{m2}}{C_L} = \frac{\tan \phi \cdot g_{m1} g_{m2} R_1 R_2}{g_{m2} R_1 R_2 C_L}$$

$$C_C = C_L \frac{g_{m1}}{g_{m2}} \tan \phi$$



* Design, 100MHz unity gain amp. to derive $C_L = 10\text{pF}$.
 $\phi = 45^\circ$.

$$\therefore C_C = 10\text{pF}$$

$$\therefore 100\text{MHz} \times 2\pi \times C_C = g_{m1}$$

$$2 \times 3.143 \times 10^{-12} \times 10^{-8} = g_{m1}$$

$$\therefore g_{m1} = 6.28\text{mS}$$

Suppose you are allowed to use 1mA current.
differential two stages
each device is allowed for $\frac{1}{4}\text{mA}$.

$$\therefore g_m = \sqrt{\mu C_{ox} \frac{W}{L} 2I_D}$$

\therefore if techno is known.

~~g_m~~ W/L is fixed.

* if two stages are not identical

ie. $g_{m1} = \frac{1}{2} g_{m2}$

$$\therefore C_c = \frac{1}{2} C_L = 5\text{pF}.$$

$$g_{m1} = 3\text{mS}.$$

at you will choose the ratio of currents b/w devices.

* if 1st stage is $\frac{1}{100}$ as powerful as 2nd stage.

$C_c \rightarrow$ quite small.

assumptions in equations

C_c is large are no more valid.

choice 65 nm 5T techno / choose on your own.

a) → optimal in power consumption
or

b) optimal in Area.
or

c) optimal in power supply voltage.

unity gain bandwidth

$$\text{unity Band.} = 200 \text{ MHz}$$

$$C_L = 10 \text{ pF}$$

$$\phi = 60^\circ$$

gain_{dc} → should be more than 400
or 50dB.

$G(s)$

0

$$i_n = +g_m v_n$$

$$v_n = i_n R_i - R_i i_n$$

$$i_n = +g_m (v_n - i_n R_i)$$

$$i_n = g_m v_n - g_m i_n R_i$$

$$i_n [1 + g_m R_i] = v_n g_m$$

$$R_o \frac{i_n}{v_{in}} = \frac{g_m R_o}{1 + g_m R_i} = \text{gain}$$