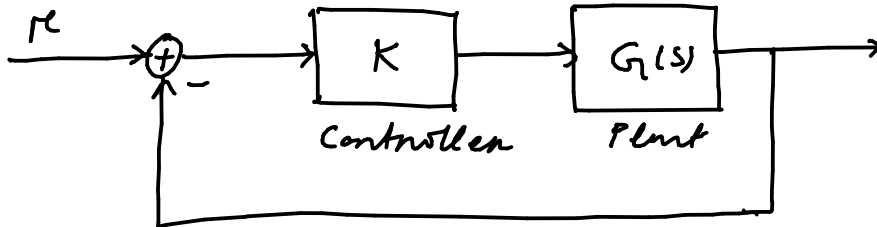


ELL225

Lecture - 25

Nyquist contour mapping

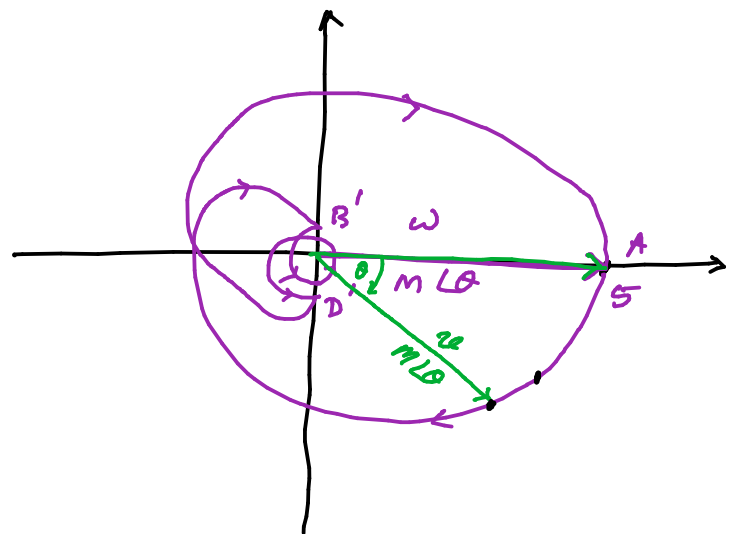
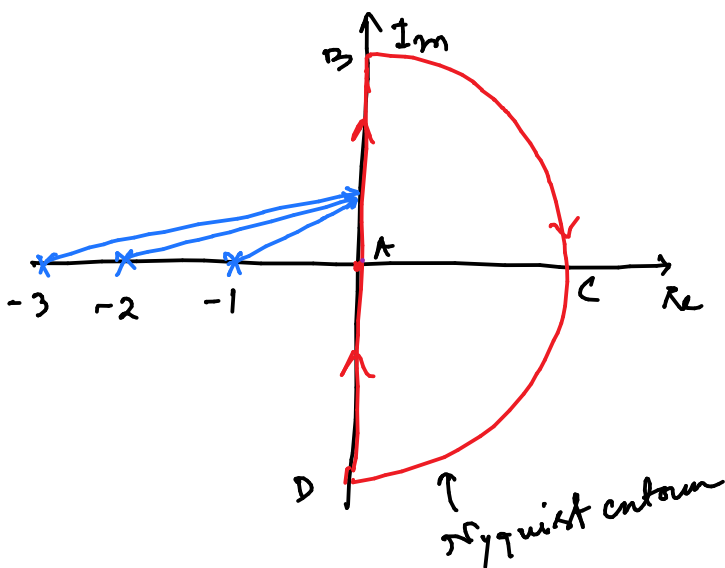


$$v = \check{F}(s) = KG(s)$$

$$v = x + jy = M \angle \theta$$

$$\text{Let } G(s) = \frac{30}{(s+1)(s+2)(s+3)}$$

Assume that $K = 1$



At point A

$$M = \frac{30}{1 \times 2 \times 3} = 5$$

$$\theta = 0^\circ$$

For $A \rightarrow B$

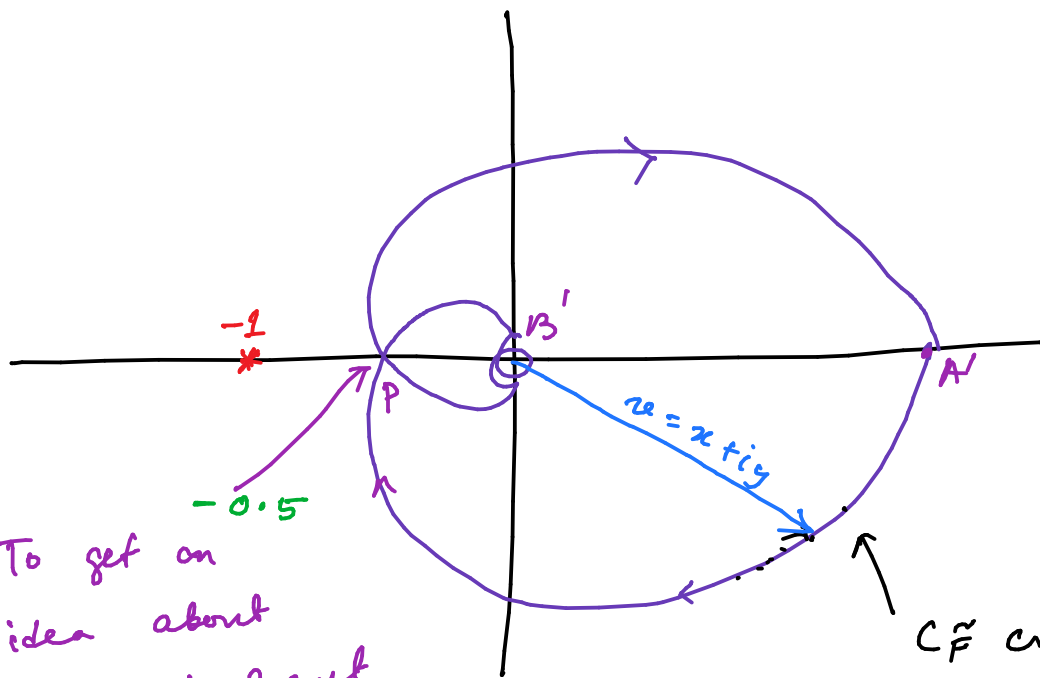
$$\begin{aligned} \theta &= -\theta_{P_1} - \theta_{P_2} - \theta_{P_3} \\ &= -270^\circ \end{aligned}$$

From B-D

M is very small

$$\begin{aligned}\theta &= -(-180^\circ) - (-180^\circ) - (-180^\circ) \\ &= 3 \times 180 \\ &= 540\end{aligned}$$

→ When we study stability the mapped Nyquist contour from B to D (having ∞ radius) does not contribute for encirclement about point -1 .
(since its magnitude is very small & the contour remains very close to the origin)



To get an idea about the encirclement

of point -1 , we need to compute the point P .

C.F. contour of Nyquist plot

$$G(j\omega) = \frac{30}{(1+j\omega)(2+j\omega)(3+j\omega)}$$

why s is replaced with only $j\omega$ instead of $\sigma + j\omega$?

Since we are moving

from A to B , $\sigma = 0$

To evaluate point P , where $v = x + jy$ has 0 imaginary part, we will make the imaginary part of $G(j\omega)$ to 0.

$$v = G(j\omega) = 30 \left[\frac{(1-j\omega)(2-j\omega)(3-j\omega)}{(1+j\omega)(1-j\omega)(2+j\omega)(2-j\omega)(3+j\omega)(3-j\omega)} \right]$$

$$= 30 \left[\frac{6 - 6\omega^2 + j\omega^3 - j11\omega}{(1+\omega^2)(4+\omega^2)(9+\omega^2)} \right]$$

$$N = G(j\omega) = 30 \left[\underbrace{\frac{6 - 6\omega^2}{(1+\omega^2)(4+\omega^2)(9+\omega^2)}}_x + j \underbrace{\frac{\omega^3 - 11\omega}{(1+\omega^2)(4+\omega^2)(9+\omega^2)}}_y \right]$$

set $y = 0$

then $\omega^3 - 11\omega = 0$

$$\Rightarrow \omega^2 = 11 \quad \omega = \sqrt{11}$$

At $\omega = \sqrt{11}$ the vector $\omega = x + jy$ has reached at point P.

• Then the real part of $\omega = x + jy$ at point P

is $G(j\omega) = 30 \left[\frac{6 - 66}{12 \times 15 \times 20} \right] = -0.5$



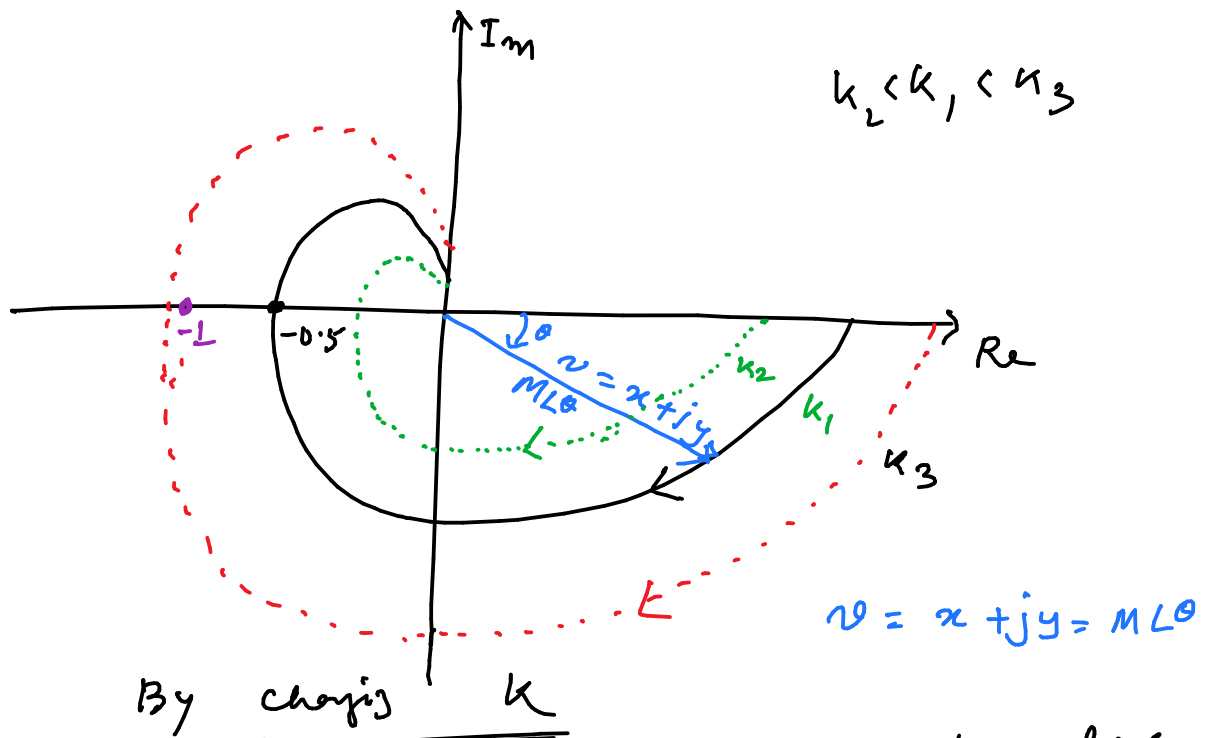
There is no encirclement about the point $-1 \pm j0$ by Nyquist plot on C_F contour.

$$Z = P + N$$

$$= 0 + 0$$

$\Rightarrow z = 0 \Rightarrow$ The closed loop system for $K = 1$ is stable, which follows from Nyquist stability criterion.

\rightarrow We will now vary the gain K .



the magnitude of v will change
& the angle θ will remain same.

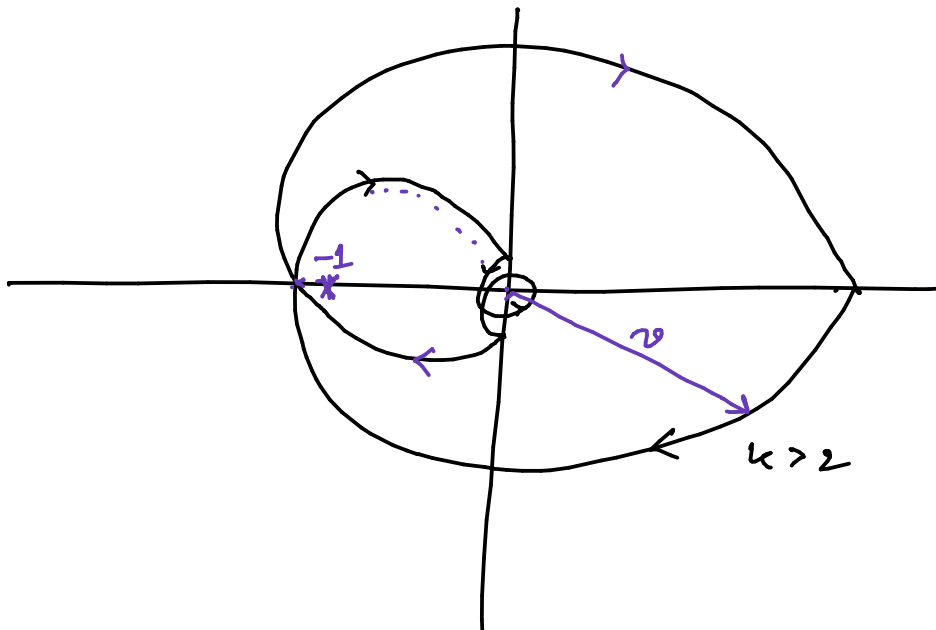
The closed loop system will remain stable as long as there is no encirclement of point $-1 \pm j0$ for choosing k .

- For $0 < k \leq 2$ there will be no encirclement about point -1
- For $k > 2$ there will be encirclement of point -1 .

BIBO stable

→ Point P for $k < 2$ will be greater than -1

Point P for $k > 2$ will be less than -1



$$N = 2$$

$$Z = P + N$$

$$= 0 + 2$$

$= 2$ which is unstable.

→ Gain Margin (G.M.)

$$v = \tilde{F}(j\omega) = M L^{\theta}$$

$$M = |\tilde{F}(j\omega)| = \eta$$

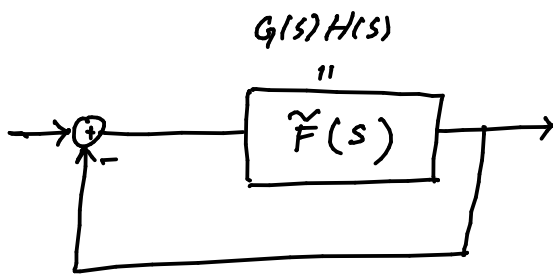
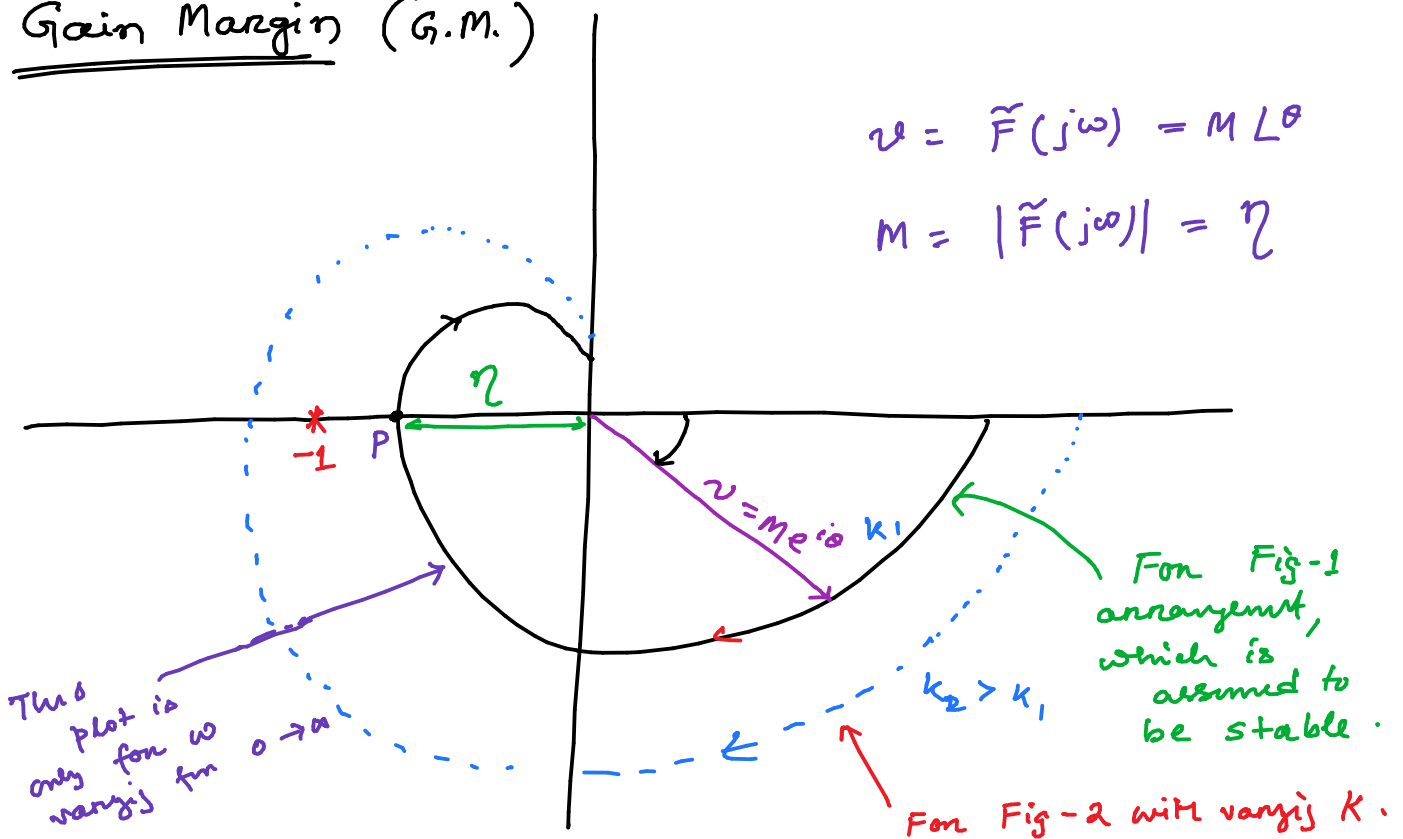


Fig - 1

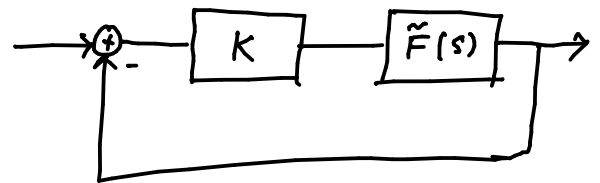


Fig-2

- By changing the parameter $K > 0$, one can make the Nyquist plot to encircle point $-1, 2$ hence change the stability property (stable \rightarrow unstable).

→ At point P, we have $|v| = |\tilde{F}(j\omega)| = \eta$

gain of $\tilde{F}(j\omega) = G(j\omega)H(j\omega)$

⇓

- If we change the gain of $\tilde{F}(j\omega)$ by

an amount of $\frac{1}{|\tilde{F}(j\omega)|} = \frac{1}{\eta}$, then

system will be in the verge of instability.

• Gain Margin : It is the amount of gain change required of $\tilde{F}(j\omega) = G(j\omega)H(j\omega)$ at

the phase angle $\theta = -180^\circ$ such that

$$\theta = \angle \tilde{F}(j\omega)$$

The point where Nyquist plot crosses -ve real axis.

the closed loop system become

(BIBO) unstable (the Nyquist plot will pass through the point $-1 \pm j0$).

|||

The reciprocal of gain $|\tilde{F}(j\omega)|$ at the frequency (denoted as ω_π) at which the phase angle $\theta = -180^\circ$.

|||

$$\text{Gain margin} = \frac{1}{|\tilde{F}(j\omega_\pi)|}$$

↓
usually defined in terms of decibel

↓

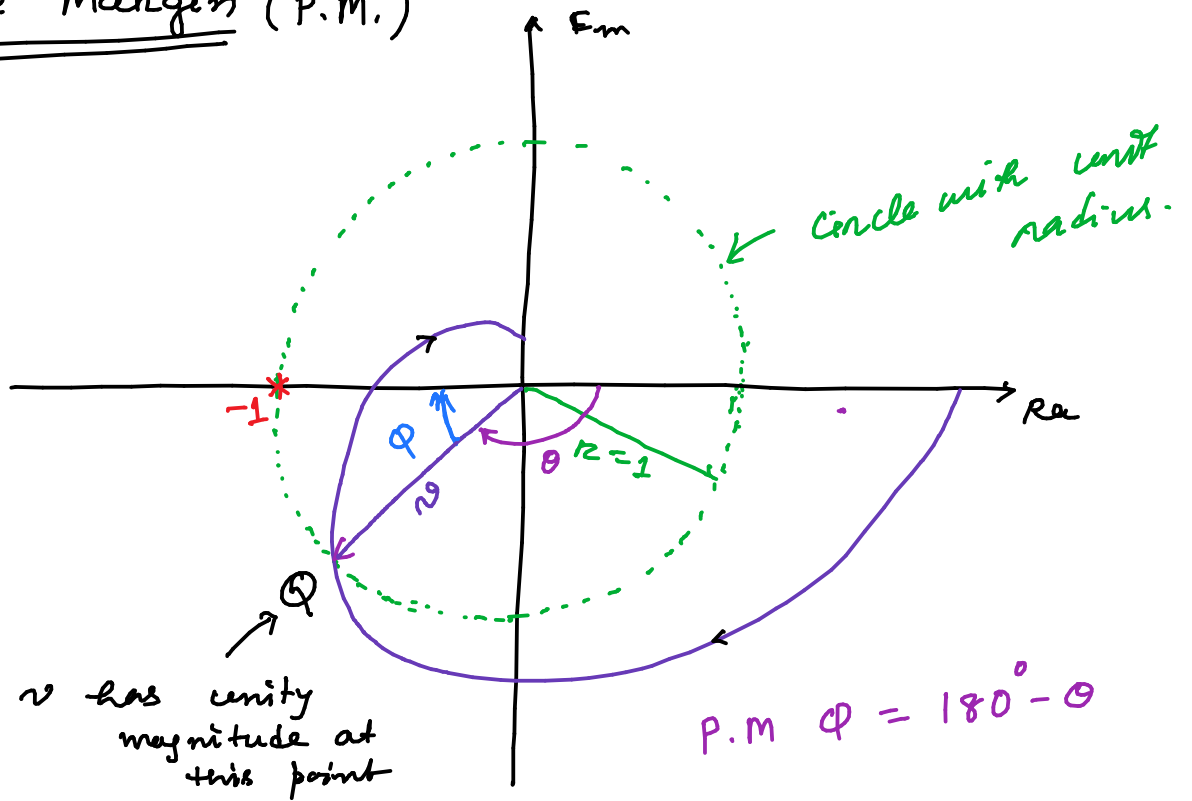
$$\begin{aligned} \text{Hem Gain margin} &= 20 \log \left(\frac{1}{\eta} \right) \\ &= -20 \log \eta \text{ dB} \end{aligned}$$

$$\text{where } \eta = |\tilde{F}(j\omega_\pi)|$$

• ω_π : Phase cross-over frequency.

• Depending upon the value of η , the G.M. could be +ve or -ve (see the "log" function property).

• Phase Margin (P.M.)



One can make the system unstable by changing the phase angle θ of $\tilde{F}(j\omega)$ at unity gain.



For instance, in the above figure, if we hold the point Q & rotate it by an angle ϕ in clockwise direction then the system will be in the range of instability, i.e. the Nyquist plot will pass through the point -1 . Hence phase margin is defined as follows:

- Phase margin : It is the amount of phase shift of $\tilde{F}(j\omega)$ is required at unity gain ($|\tilde{F}(j\omega)|=1$) to make the closed loop system unstable. On the Nyquist plot pass through the point $-1 \pm j0$.

on

The amount of angle that the Nyquist plot of $\tilde{F}(j\omega)$ must be rotated so that the unity magnitude point ($|\tilde{F}(j\omega)|=1$, Q-point) will pass through the point $-1 \pm j0$.

- * The G.M. & P.M. give quantitative measure of closed loop system stability (measures for distance to closed loop instability).

→ Let ω_u be the frequency at which

$$|\tilde{F}(j\omega_u)| = 1 \quad (\text{Q-point})$$

ω_u : Gain cross-over frequency.

on the previous fig :

$$-\theta - \phi = -180^\circ$$

$$\Rightarrow \phi = 180^\circ - \theta \quad \leftarrow \text{Phase margin}$$

Example :

$$G(s) = \frac{5}{s(s+1)(s+5)}$$

$$G(j\omega) = \frac{5}{(j\omega)(j\omega+1)(j\omega+5)}$$

$$= \frac{5(-j\omega)(1-j\omega)(5-j\omega)}{\omega^2(1+\omega^2)(25+\omega^2)}$$

$$-j5\omega(5-j\omega-j5\omega-\omega^2)$$

$$= -j25\omega - 5\omega^2 - 25\omega^2 + j5\omega^3$$

$$= -\frac{30\omega^2}{\omega^2(1+\omega^2)(25+\omega^2)} + j\frac{5\omega(\omega^2-5)}{\omega^2(1+\omega^2)(25+\omega^2)}$$

Negative Real axis cross) $\text{Im}(\cdot) = 0$

$$\Rightarrow 5\omega(\omega^2-5) = 0$$

$$\omega = \pm\sqrt{5} \rightarrow \omega = \sqrt{5}$$

(15.25)

$$\text{Re}(G(j\sqrt{5})) = -\frac{150}{5 \times 6 \times 30} = -\frac{1}{6}$$

$$\text{So } \eta = 0.167$$

$$G.M. = -20 \log \eta = -20 \log(0.167) = 15.55 \text{ dB}$$

• To compute P.M., we need to find ω for

which $|G(j\omega)| = 1$

$$\Rightarrow \left[\frac{30\omega^2}{\omega^2(1+\omega^2)(25+\omega^2)} \right]^2 + \left[\frac{5\omega(\omega^2-5)}{\omega^2(1+\omega^2)(25+\omega^2)} \right]^2 = 1$$

Needs \uparrow to solve for ω (Computer may help you)

It is computed that for $\omega = 0.78$ we

$$\text{have } |G(j\omega)| \cong 1.$$

Hence for $\omega = 0.78$, we need to

compute $\angle G(j\omega)$

* Following rules may be used for $\tan^{-1}(\cdot)$: For complex no. $\sigma + j\omega$

$$\theta = \begin{cases} \tan^{-1}\left(\frac{\omega}{\sigma}\right), & \text{for } \sigma > 0, \omega > 0 \text{ (1st \& 4th quadrant)} \\ \tan^{-1}\left(\frac{\omega}{\sigma}\right) + \pi, & \text{for } \omega \geq 0, \sigma < 0 \text{ (2nd quadrant)} \\ \tan^{-1}\left(\frac{\omega}{\sigma}\right) - \pi, & \text{for } \omega < 0, \sigma < 0 \text{ (3rd quadrant)} \\ \pi/2, & \text{for } \omega > 0, \sigma = 0 \\ -\pi/2, & \text{for } \omega < 0, \sigma = 0 \end{cases}$$

For our case:

evaluating $G(j\omega)$ at $\omega = 0.78$

$$G(j\omega) = - \frac{30\omega^2}{\omega^2(1+\omega^2)(25+\omega^2)} + j \frac{5\omega(\omega^2-5)}{\omega^2(1+\omega^2)(25+\omega^2)}$$

$$= - \frac{18 \cdot 252}{25 \cdot 059} + j \left(\frac{-17 \cdot 12}{25 \cdot 059} \right)$$

Hence,

$$\begin{aligned} \angle G(j\omega) &= \tan^{-1}\left(\frac{17 \cdot 12}{18 \cdot 252}\right) - \pi \\ &= 43.167 - 180 \\ &= -136.83 \end{aligned}$$



To compute P.M.:

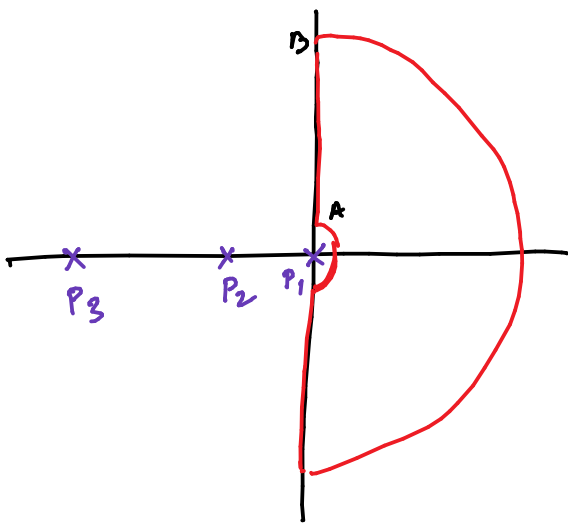
$$\boxed{-136.83 - \phi = -180^\circ}$$

$$\Rightarrow \phi = 43.17^\circ$$



43.17° additional phase shift required for $\tilde{F}(j\omega) = G(j\omega)$, so that the Nyquist plot of $\tilde{F}(j\omega)$ will pass through $-1 \pm j0$ & make the closed loop system (B/30) unstable.

\Rightarrow Phase Margin $\phi = 43.17^\circ$



Point A $\rightarrow \theta = -90^\circ$

$M \approx \infty$

From A \rightarrow B

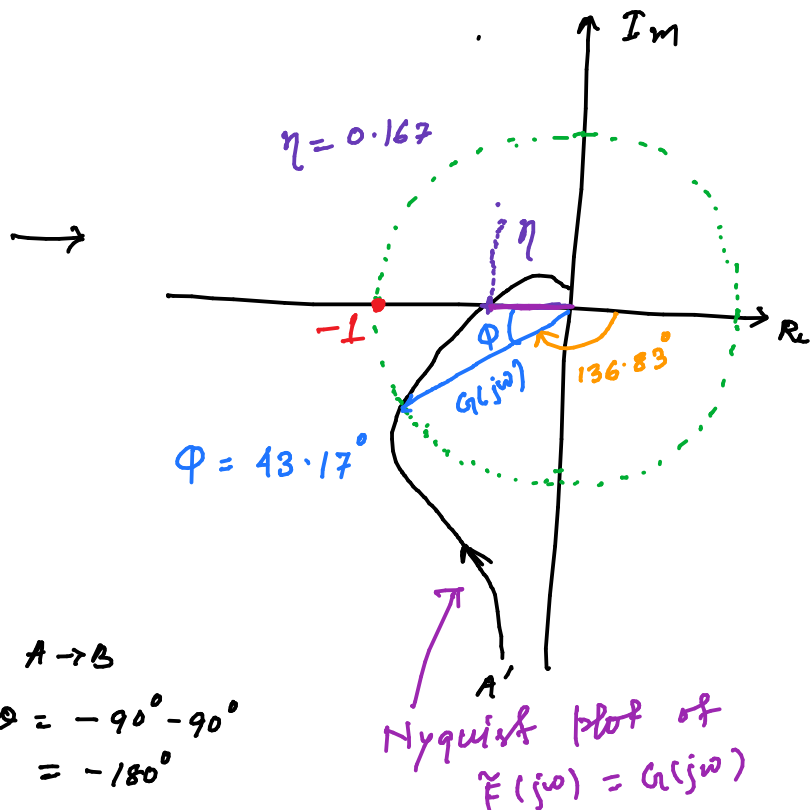
$$\begin{aligned} \theta &= -90^\circ - 90^\circ \\ &= -180^\circ \end{aligned}$$

$\angle G(j\omega)$ can also be calculated according to our standard procedure:

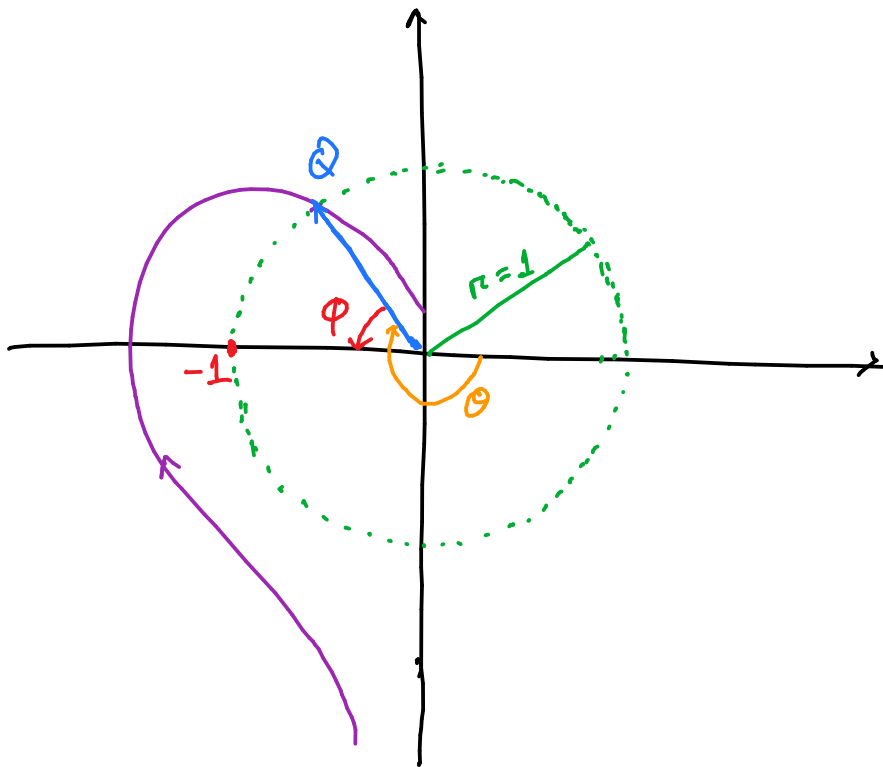
$$\begin{aligned} \angle G(j\omega) &= -\theta_{p_1} - \theta_{p_2} - \theta_{p_3} \\ &= -90^\circ - \tan^{-1}(\omega) - \tan^{-1}\left(\frac{\omega}{5}\right) \end{aligned}$$

For $\omega = 0.78$

$$\begin{aligned} \angle G(j\omega) &= -90^\circ - 37.95^\circ - 8.86^\circ \\ &= -136.81^\circ \end{aligned}$$



Nyquist plot of $\tilde{F}(j\omega) = G(j\omega)$

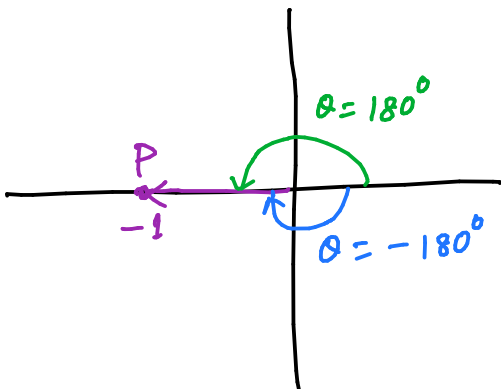


The point Q needs to be rotated an amount of ϕ° in counter-clockwise directⁿ to make the Nyquist plot pass through point -1 .

$$-\theta + \phi = -180^\circ$$

$$\Rightarrow \phi = \theta - 180^\circ$$

Phase margin.



The point P has magnitude 1 & angle $\theta = \pm 180^\circ$, depending upon the considered directⁿ of rotation of vector $-1 + j0$.

Here for defining G.M & P.M. the crucial phase angle -180° that we are considering, can also be considered as 180° .

For instance

$$-\theta + \phi = 180^\circ \quad (\text{in 2d fig for P.M.})$$

P.M. $\Rightarrow \phi = 180^\circ + \theta$