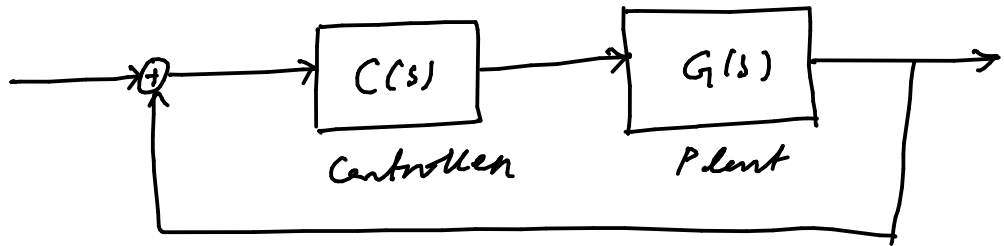


Lecture - 34

- Eliminate S.S.E (Use PI controller)

$$C(s) = K_p + \frac{K_i}{s}$$

- Reduce the S.S.E. (Use Lag compensator)

$$C(s) = \frac{K(s+z_c)}{(s+p_c)}$$

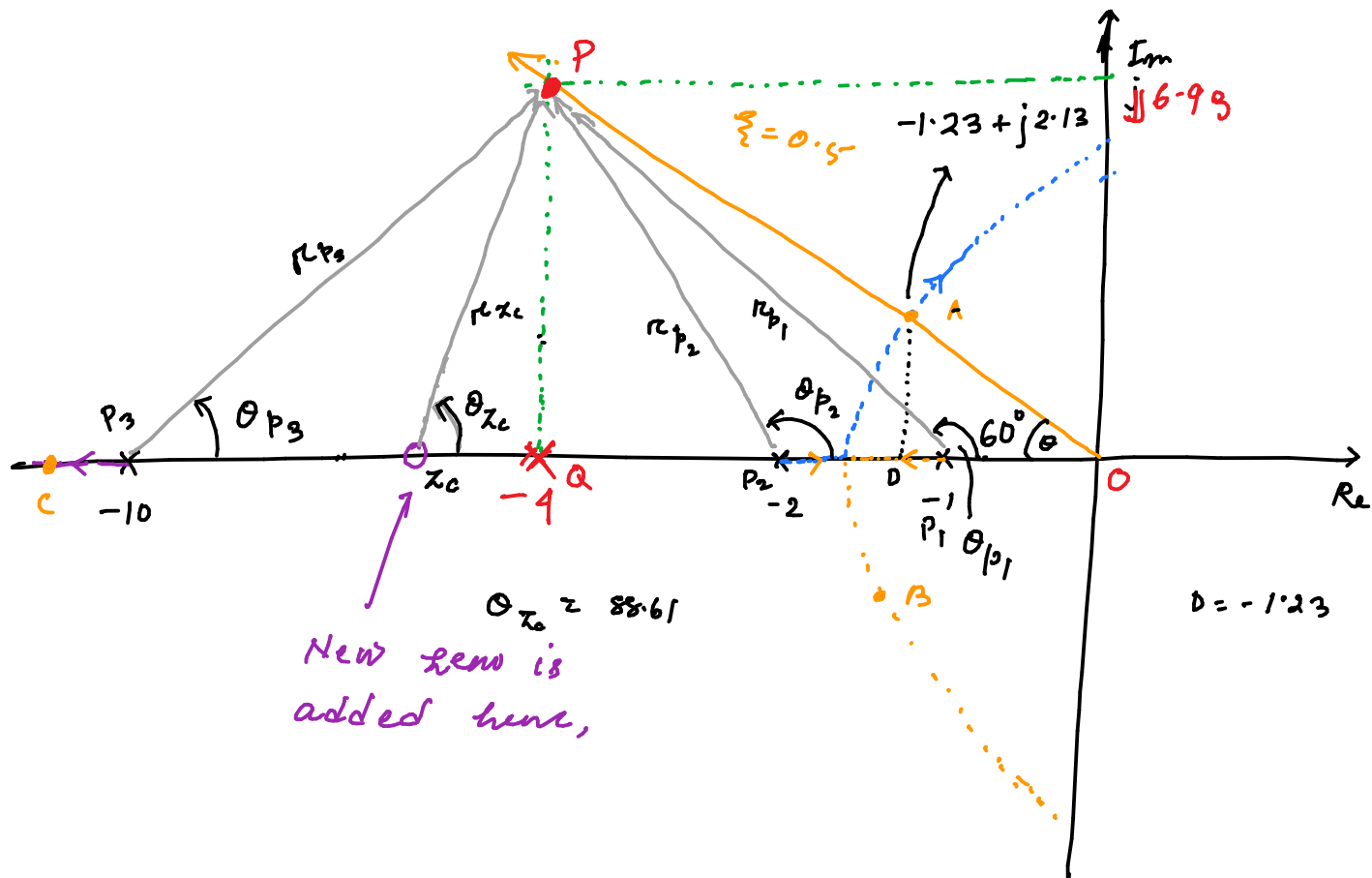
→ Achieving / Improving Transient behaviour:

- Specifications:
- Damping ratio
  - Settling time

Ex: Plant  $G(s) = \frac{1}{(s+1)(s+2)(s+10)}$

Design requirements:

- Damping ratio  $\zeta = 0.5$
- Settling time  $T_s = 1 \text{ sec.}$



Damping ratio  $0.5 \rightarrow \cos \theta = 0.5$   
 $\Rightarrow \theta = 60^\circ \checkmark$

Change gain  $K$ . S.t. the closed loop poles are at loc<sup>n</sup> (A, B, C)

$\Downarrow$

The system response, which is dominated by a pair of complex conjugate poles (A, B), will satisfy the damping ratio  $\zeta = 0.5$ .

- With respect to the new locations of closed loop poles (at A, B, C), the effect of pole at C is very small on the output response in comparison to the dominant complex conjugate pair at A, B.

At  $(A, B, C)$  pair of closed loop poles  
the settling time :

$$T_s = \frac{4}{\zeta \omega_n} \approx \frac{4}{\sigma_d} \approx \frac{4}{1.23} = 3.25 \text{ sec.}$$

• If we use only proportional controller  
then we have achieved appropriate  $\zeta = 0.5$   
but Not achieved specified settling time  $T_s$ .

We need  $T_s = 1 \text{ sec.}$

$$\Rightarrow T_s \approx \frac{4}{\sigma_d} = 1$$

$$\Rightarrow \sigma_d = 4 \quad \Downarrow$$

We need a pair of  
complex conjugate closed loop  
poles, whose real part

$$\sigma_d = -4$$

$$OQ = 4$$

$$PQ = OQ \tan 60^\circ$$

$$= 6.93$$

- To achieve  $\zeta = 0.5$  &  $T_s = 1 \text{ sec.}$  we  
need our root locus to pass through the point  
P.

→ To make the root locus pass through pt. P  
we must examine the angle criterion.

Since in the uncompensated system  
the root locus does not pass through P

⇓

$$-\theta_{p_1} - \theta_{p_2} - \theta_{p_3} \neq (2k+1)180^\circ$$

$$\theta_{p_3} = \tan^{-1}\left(\frac{PQ}{QC}\right) = \tan^{-1}\left(\frac{6 \cdot 93}{6}\right) = 49.11^\circ$$

$$\theta_{p_1} = 180^\circ - \tan^{-1}\left(\frac{6 \cdot 93}{3}\right) = 113.4^\circ$$

$$\theta_{p_2} = 180^\circ - \tan^{-1}\left(\frac{6 \cdot 93}{2}\right) = 106.1^\circ$$

• At point P

$$-\theta_{p_1} - \theta_{p_2} - \theta_{p_3} = -268.61 \neq (2k+1)180^\circ$$

Now let us introduce a zero at  
 $z_c$  (exact loc. will be computed)

At point P:

$$0 = \theta_{z_c} - \theta_{p_1} - \theta_{p_2} - \theta_{p_3} = -180^\circ$$

$$\Rightarrow \theta_{z_c} = -180^\circ + 268.61 = 88.61^\circ$$

$$\frac{6 \cdot 93}{z_c - 4} = \tan 88.61$$

$$\frac{PQ}{Qz_c} = \tan 88.61 \Rightarrow \frac{6.93}{z_c - 4} = \tan 88.61$$

$$\Rightarrow z_c \approx 4.16$$

↓

The zero loc<sup>n</sup> will be at  $-4.16$

$$z_c = -4.16$$

We implement a controller as follows

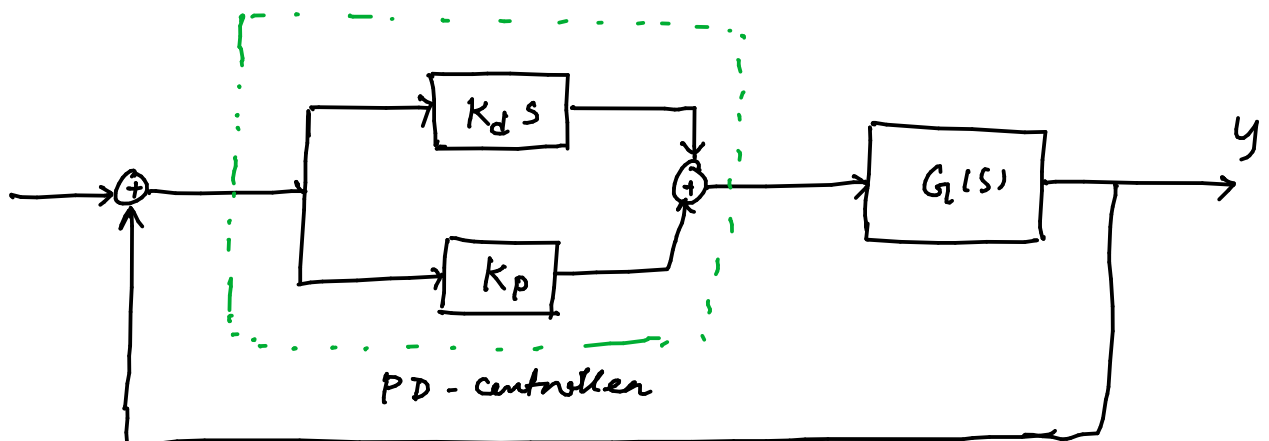
$$C(s) = K_p + K_d s$$

$$= K_d \left( s + \frac{K_p}{K_d} \right)$$

$$K_d (s + z_c)$$

Proportional-plus-derivative  
controller

PD-controller



At point P, the gain should be 1.

we need to change gain K s.t.

$$K = \frac{\prod p_1 \prod p_2 \prod p_3}{\prod z_c} = \frac{7.2 \times 7.55 \times 9.16}{6.932}$$

$$\frac{K \prod z_c}{\prod p_1 \prod p_2 \prod p_3} = 1$$

$$= 71.93 = K_d$$

$$z_c = -4.16$$

$$\text{Controller } C(s) = K_d (s + z_c)$$

$$= 71.93 (s + (4.16 \times 71.93))$$

$$\left( \begin{array}{l} \frac{K_p}{K_d} = 4.16 \\ \Rightarrow K_p = 4.16 \times K_d \end{array} \right.$$

$$C(s) = \frac{71.93}{K_d} \left( s + \frac{4.16 \times 71.93}{71.93} \right)$$

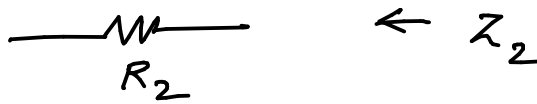
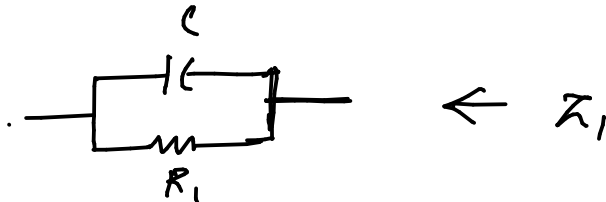
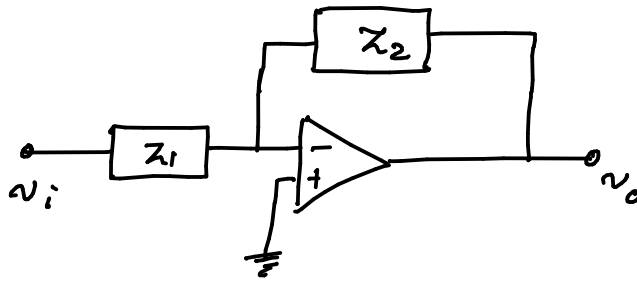
With this compensation, the root-locus will pass through point P. In turn in the closed loop we will have

$$\left\{ \begin{array}{l} \zeta = 0.5 \\ T_s = 1 \text{ sec.} \end{array} \right.$$

\* With the PD controller, we can (approximately) achieve the specified transient response, however, the steady state error may not go to zero.

Check the SSE for the considered example in "SISOTOOL" in MATLAB.

→ Circuit Realization for PD Controller :



$$G_c(s) = - \frac{V_o(s)}{V_i(s)}$$
$$= -R_2 C \left( s + \frac{1}{R_1 C} \right)$$