

When this feedback interconnection is "well-posed" or "well-defined"

$$H_1(s) = \frac{s-1}{s+2} \quad H_2(s) = 1$$

$$\left[ \frac{1}{1 - H_1(s)H_2(s)} \right] = \frac{s+2}{3} \leftarrow \text{improper t.f}$$

Improper t.f. are not physically realizable

∴ using analog circuits

st. is not possible

to write in  $\begin{cases} \dot{x} = Ax + bu \\ y = cx \end{cases}$  form

$$H_1 = \frac{s+2}{s+1} \quad H_2 = \frac{s+1}{s+2}$$

$$\frac{1}{1 - H_1 H_2} = \frac{1}{0}$$

External / input signals :  $r_1, r_2$

internal / output signals :  $e_1, y_1, e_2, y_2$

$$\text{t.f for } r_1 \text{ to } e_1 = \frac{1}{1 - H_1 H_2}$$

$$r_1 \text{ to } y_1 = \frac{H_1}{1 - H_1 H_2}$$

For the feedback system input-output map

(2)

$$\begin{bmatrix} e_1 \\ e_2 \\ y_1 \\ y_2 \end{bmatrix} = \underbrace{\begin{bmatrix} (1 - H_1 H_2)^{-1} & (1 - H_1 H_2)^{-1} H_2 \\ (1 - H_1 H_2)^{-1} H_1 & (1 - H_1 H_2)^{-1} \\ (1 - H_1 H_2)^{-1} H_1 & (1 - H_1 H_2)^{-1} H_1 H_2 \\ (1 - H_1 H_2)^{-1} H_2 H_1 & (1 - H_1 H_2)^{-1} H_2 \end{bmatrix}}_{\text{closed loop t.f.}} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix}$$

closed loop t.f.

$H(s)$

There are 4 different transfer functions

$$(1 - H_1 H_2)^{-1}, \quad (1 - H_1 H_2)^{-1} H_1, \quad (1 - H_1 H_2)^{-1} H_2, \quad (1 - H_1 H_2)^{-1} H_1 H_2$$

$(1 - H_1 H_2)^{-1} \leftarrow$  plays a crucial role.

\_\_\_\_\_ x \_\_\_\_\_

Some notations:

$\mathbb{R}[s]$   $\leftarrow$  the set of polynomials having coefficients in  $\mathbb{R}$

$$\mathbb{R}(s) := \left\{ g(s) \mid g(s) = \frac{n(s)}{d(s)}, \quad n(s) \in \mathbb{R}[s], \quad d(s) \in \mathbb{R}[s], \quad d(s) \neq 0 \right\}$$

$\uparrow$  set of real rational functions

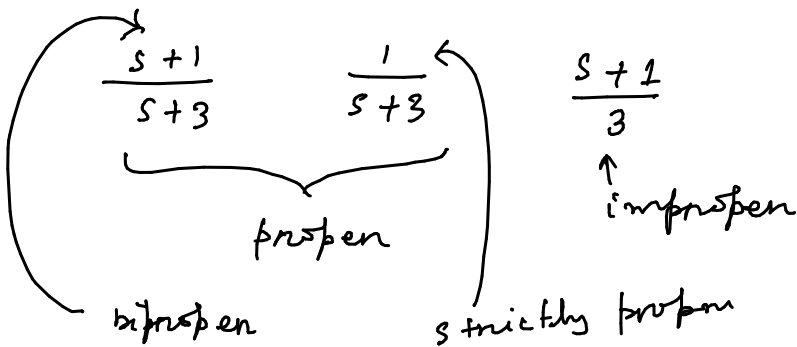
$$\delta_a(g(s)) := \deg(d(s)) - \deg(n(s))$$

$\exists f \quad \delta_\infty(g(s)) > 0 : g(s)$  is proper real rational funct?

$\delta_\infty(g(s)) > 0 : g(s)$  is strictly proper

$\delta_\infty(g(s)) = 0 : g(s)$  is biproper

$\delta_\infty(g(s)) < 0 : g(s)$  is improper



$\lim_{s \rightarrow \infty} (g(s))$  when  $g(s)$  are as above.

$\lim_{s \rightarrow \infty} \frac{s+1}{s+3} = 1$

$\lim_{s \rightarrow \infty} \frac{1}{s+3} = 0$

proper  $\rightarrow \lim_{s \rightarrow \infty} g(s) = d$

when  $d$  is a real number.

$\times \lim_{s \rightarrow \infty} \frac{s+1}{3} = \infty \leftarrow$  improper t.f.

$\lim_{s \rightarrow \infty} g(s) = d \quad d \in \mathbb{R} \leftarrow$  proper

$\exists f \quad d = 0$  then  $g(s)$  is strictly proper

$d \neq 0$  then  $g(s)$  is biproper

$\frac{s+1}{s+3} = 1 + \left( \frac{\tilde{g}(s)}{s+3} \right)$   
 $\subset$  strictly proper.

$$(1 - H_1 H_2)^{-1}, (1 - H_1 H_2)^{-1} H_1, (1 - H_1 H_2)^{-1} H_2, (1 - H_1 H_2)^{-1} H_1 H_2$$

(4)

$(1 - H_1 H_2)$  : inverse exists & inverse is a proper transfer fun<sup>n</sup>.

For well-defined feedback interconnection we need : Above 4 t.f.s to be proper.

$$(1 - H_1 H_2)^{-1} \rightarrow \frac{s+1}{s-1} \rightarrow \frac{s-1}{s+1} ( )$$

$$H_1(s) \rightarrow \begin{cases} \dot{x}_1 = A_1 x_1 + b_1 u_1 \\ y_1 = c_1 x_1 + d_1 u_1 \end{cases}$$

$$H_2(s) \rightarrow \begin{cases} \dot{x}_2 = A_2 x_2 + b_2 u_2 \\ y_2 = c_2 x_2 + d_2 u_2 \end{cases}$$

$$\lim_{s \rightarrow \infty} H_1(s) = d_1 \rightarrow H_1(s) = \frac{c_1 (sI - A_1)^{-1} b_1 + d_1}{1} \leftarrow \in \mathbb{R}$$

↑  
strictly proper.

→ Well-posed : If all the above 4 t.f.s are proper (physically realizable)

|||

The t.f  $(1 - H_1 H_2)^{-1}$  exists & it is proper.

→ Result : The feedback interconnection is well-posed iff

$$\lim_{s \rightarrow \infty} (1 - H_1(s)H_2(s)) \neq 0 \equiv (1 - d_1d_2) \neq 0$$

((1 - d\_1d\_2) is invertible)

For well-posedness condition is equivalent to

$$(1 - H_1H_2)^{-1} \text{ exists \& is proper.}$$

- ①  $(1 - H_1H_2)^{-1}$  exists & is proper  $\Rightarrow 1 - d_1d_2 \neq 0$
- ②  $1 - d_1d_2 \neq 0 \Rightarrow (1 - H_1H_2)^{-1}$  exists & is proper

Above two statements we have to show.

① let  $(1 - H_1H_2)^{-1}$  exists & is proper.

Existence of  $(1 - H_1H_2)^{-1} \Rightarrow$  numerator of  $(1 - H_1H_2)$  is not zero polynomial.

⊗  $\left\{ \begin{aligned} &(1 - H_1H_2)^{-1} \text{ is proper} \Rightarrow \text{The degree of numerator} \\ &\text{of } (1 - H_1H_2)^{-1} \text{ is less or equal to degree of} \\ &\text{denominator of } (1 - H_1H_2)^{-1}. \end{aligned} \right.$

⊗  $\left\{ \begin{aligned} &\text{Since } H_1 \& H_2 \text{ are proper, } (1 - H_1H_2) \text{ is also proper.} \\ &\Rightarrow \text{the degree of numerator of } 1 - H_1H_2 \text{ is less or} \\ &\text{equal to the degree of denominator of } 1 - H_1H_2 \end{aligned} \right.$

$$\left( 1 - H_1H_2 = \left( 1 - \frac{b}{a} \cdot \frac{y}{z} \right) = \frac{ax - by}{ax} \quad \begin{matrix} \nearrow \\ \text{deg}(by) \leq \text{deg}(ax) \end{matrix} \right)$$

From (\*) & (\*\*) statements it is clear that

$(1 - H_1 H_2)^{-1}$  is biproper, hence it can

be written as  $(1 - H_1 H_2)^{-1} = \Delta + \underbrace{\hat{h}(s)}_{\text{strictly proper}}$

where

$$\Delta = \frac{1}{1 - d_1 d_2}$$

$$\frac{2s + 1}{s + 3} = \underline{2} + \left( \frac{-5}{s + 3} \right)$$

$$\frac{s + 1}{2s + 3} = \underline{\frac{1}{2}} + \left( \frac{-1/2}{2s + 3} \right)$$

Hence  $1 - d_1 d_2 \neq 0$

• second statement ②

Let  $1 - d_1 d_2 \neq 0$ . Then

$$(1 - H_1 H_2) = (1 - d_1 d_2) + \underbrace{\hat{g}(s)}_{\text{strictly proper}}$$

Let us write  $\hat{g}(s) = \frac{\hat{b}(s)}{\hat{a}(s)}$  when  $\deg(\hat{b}(s)) < \deg(\hat{a}(s))$

$$1 - H_1 H_2 = (1 - d_1 d_2) + \frac{\hat{b}(s)}{\hat{a}(s)} = \frac{(1 - d_1 d_2) \hat{a}(s) + \hat{b}(s)}{\hat{a}(s)}$$

Since  $1 - d_1 d_2 \neq 0$ , the coefficient of highest degree  $s$  term in the numerator of  $1 - H_1 H_2$  is not zero. Hence  $(1 - H_1 H_2)^{-1}$  exists.

Further, since  $\deg(\hat{a}(s)) > \deg(\hat{b}(s))$ , and  $1 - d_1 d_2 \neq 0$ , the degree of numerator of  $1 - H_1 H_2$  is equal to the degree of denominator of  $1 - H_1 H_2$ . Hence  $1 - H_1 H_2$  is biproper  $\Rightarrow (1 - H_1 H_2)^{-1}$  is proper, in fact it is biproper.

$$H_1(s) = \begin{cases} \dot{x}_1 = A_1 x_1 + b_1 u_1 \\ y_1 = c_1 x_1 + d_1 u_1 \end{cases} \quad H_2(s) = \begin{cases} \dot{x}_2 = A_2 x_2 + b_2 u_2 \\ y_2 = c_2 x_2 + d_2 u_2 \end{cases}$$

$$e_1 = r_1 + y_2 \quad e_2 = r_2 + y_1 \quad \begin{matrix} u_1 = e_1 \\ u_2 = e_2 \end{matrix}$$

$$\dot{x}_1 = A_1 x_1 + b_1 u_1 \quad \text{--- (1)}$$

$$= A_1 x_1 + b_1 e_1 = A_1 x_1 + b_1 (r_1 + y_2) \quad \text{--- (2)}$$

$$\dot{x}_2 = A_2 x_2 + b_2 e_2 \quad \text{--- (3)}$$

$$= A_2 x_2 + b_2 (r_2 + y_1) \quad \text{--- (4)}$$

closed loop

$$\hookrightarrow \text{state } \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad \text{input} = \begin{bmatrix} r_1 \\ r_2 \end{bmatrix}$$

$$e_1 = r_1 + y_2 \\ = r_1 + c_2 x_2 + d_2 e_2$$

$$\Rightarrow e_1 - d_2 e_2 = c_2 x_2 + r_1 \quad \text{--- (*)}$$

$$e_2 = r_2 + y_1 \\ = r_2 + c_1 x_1 + d_1 e_1$$

$$\Rightarrow -d_1 e_1 + e_2 = r_2 + c_1 x_1 \quad \text{--- (**)}$$

From (\*) & (\*\*)

$$\begin{bmatrix} 1 & -d_2 \\ -d_1 & 1 \end{bmatrix} \begin{bmatrix} e_1 \\ e_2 \end{bmatrix} = \begin{bmatrix} 0 & c_2 \\ c_1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} e_1 \\ e_2 \end{bmatrix} = \begin{bmatrix} 1 & -d_2 \\ -d_1 & 1 \end{bmatrix}^{-1} \left( \begin{bmatrix} 0 & c_2 \\ c_1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix} \right)$$

- The feedback interconnection is well-posed if the internal signals  $e_1, e_2, y_1, y_2$  can uniquely be determined for every choice of system state  $x$  & the external/input signals  $r_1, r_2$ .

$$y_1 = c_1 x_1 + d_1 e_1$$

$$= c_1 x_1 + d_1 (r_1 + y_2) \quad \text{--- } \checkmark$$

$$\Rightarrow y_1 - d_1 y_2 = c_1 x_1 + d_1 r_1$$

$$y_2 = c_2 x_2 + d_2 e_2$$

$$= c_2 x_2 + d_2 (r_2 + y_1)$$

$$\Rightarrow -d_2 y_1 + y_2 = c_2 x_2 + d_2 r_2 \quad \text{--- } \checkmark$$

For  $\checkmark \checkmark$

$$\begin{bmatrix} 1 & -d_1 \\ -d_2 & 1 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} c_1 & 0 \\ 0 & c_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} d_1 & 0 \\ 0 & d_2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix}$$

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & -d_1 \\ -d_2 & 1 \end{bmatrix}^{-1} \left( \begin{bmatrix} c_1 & 0 \\ 0 & c_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} d_1 & 0 \\ 0 & d_2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix} \right)$$

So  $e_i$  &  $y_i$  for  $i=1, 2$  can uniquely be determined for given a state  $x$  & external signal  $r_1$  &  $r_2$  iff

$$\begin{bmatrix} 1 & -d_1 \\ -d_2 & 1 \end{bmatrix} \text{ invertible } \Leftrightarrow 1 - d_1 d_2 \neq 0$$



Observe that in both cases (state space and t.f) the condition for well-posedness is same.

i.e.

feedback interconnection is well-posed iff  $1 - d_1 d_2 \neq 0$  or  $1 - d_1 d_2$  is invertible.

One can similarly extend all the above results to multi-input multi-output system.